



# TRUSS ITN

Workshop

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HORIZON 2020



Training in Reducing Uncertainty  
in Structural Safety

# Sensitivity of SHM Sensors to Bridge Stiffness

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# Sensitivity of SHM Sensors to Bridge Stiffness

Theorem of Virtual Work  $\Rightarrow \delta = \int \frac{MM_u}{EI} dx \Rightarrow$  valid for statics with sensors on the bridge

Matrix representation of Theorem  $\Rightarrow \{\delta\}_{t \times 1} = [P]_{t \times n} \{J\}_{n \times 1} \Rightarrow$  where P is the matrix representing  $MM_u$  values and J is vector of  $\frac{1}{EI}$  components (reciprocal of stiffness)

$$EI_n = \frac{1}{J_n}$$



# Sensitivity of SHM Sensors to Bridge Stiffness

**Sensitivity**



$$S(i, j) = \frac{\partial u_i}{\partial J_j}$$



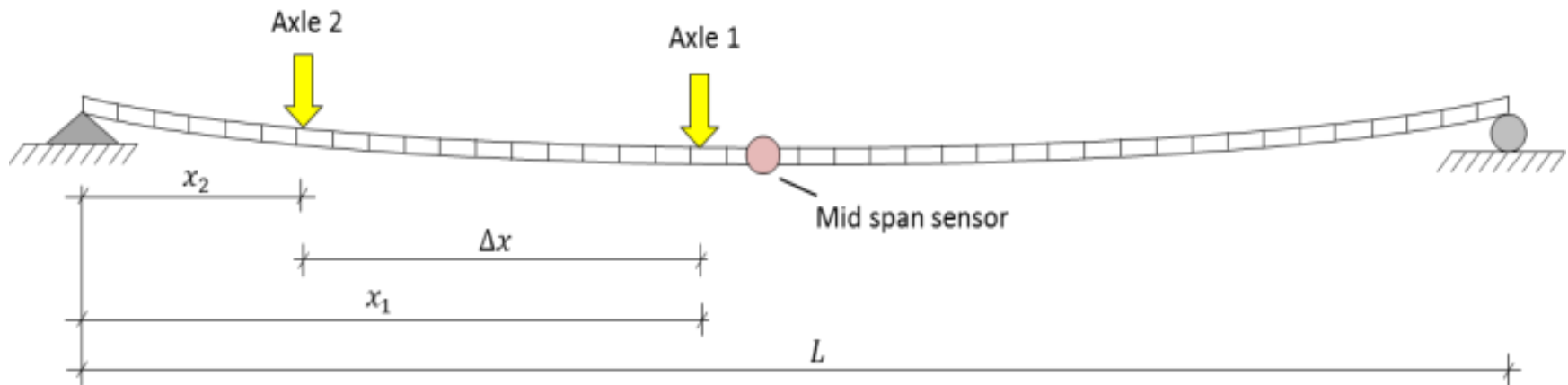
**$S(i, j)$ : Sensitivity of the deflection respect to the reciprocal of the flexural stiffness**

**$J_j$ : reciprocal of the flexural stiffness at element  $j$**



# Sensitivity of SHM Sensors to Bridge Stiffness

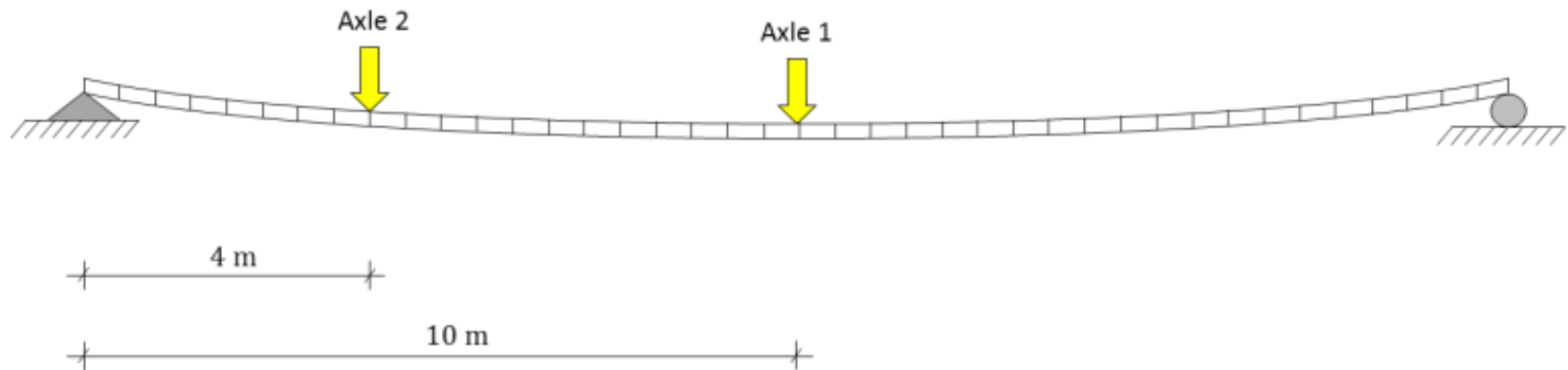
## Sensor Installation at mid span





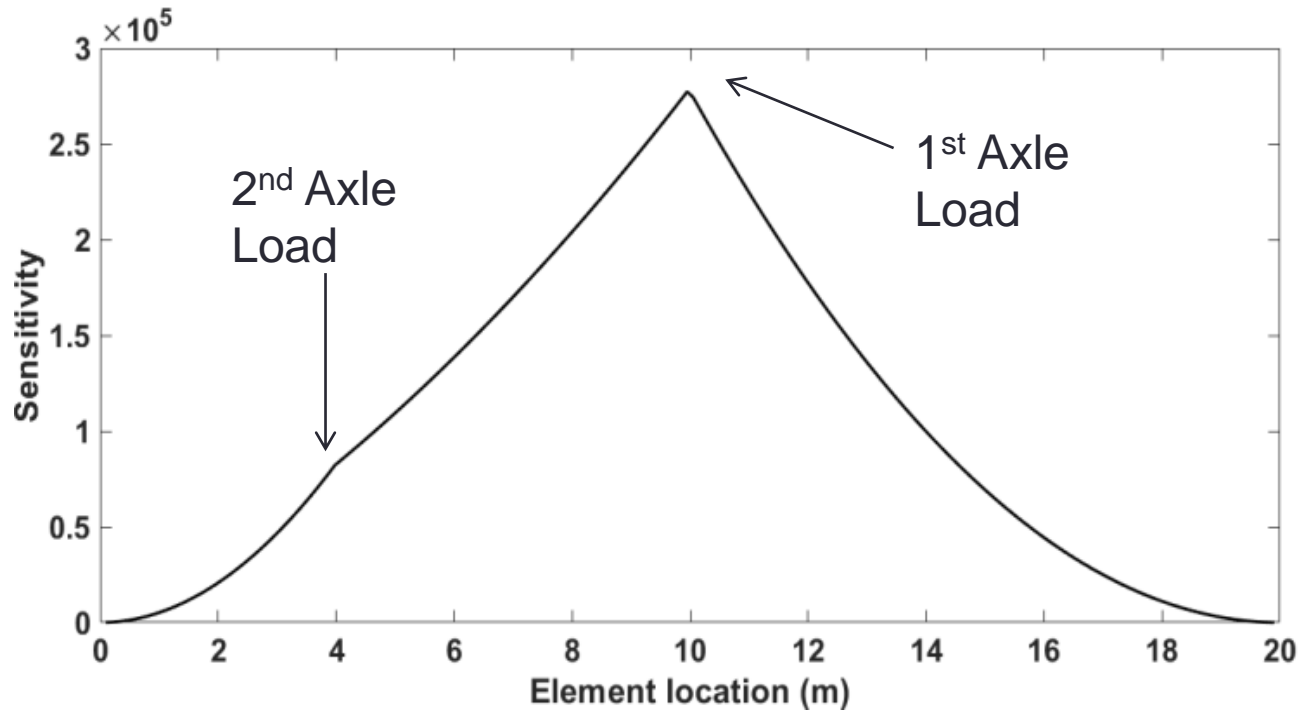
# Sensitivity of SHM Sensors to Bridge Stiffness

## Situation Analysed



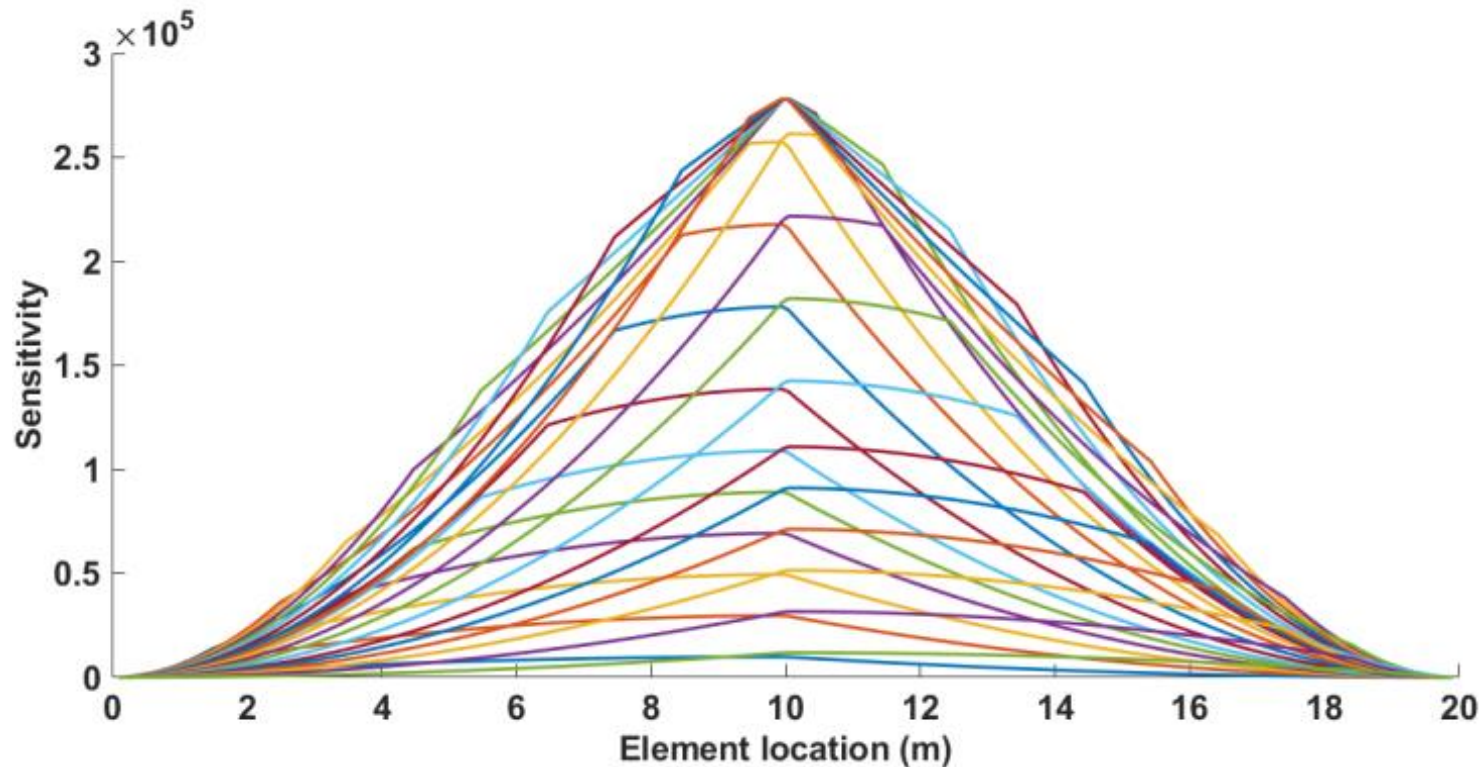


# Sensitivity of SHM Sensors to Bridge Stiffness





# Sensitivity of SHM Sensors to Bridge Stiffness



Envelope of the sensitivities





# Calculating Bridge Stiffness from deflection measurements

$$\{\delta\}_{t \times 1} = [P]_{t \times n} \{J\}_{n \times 1}$$

$$\begin{Bmatrix} \delta_1 \\ \delta_2 \\ \delta_3 \\ \delta_4 \\ \delta_5 \end{Bmatrix} = \begin{bmatrix} P_{1A} & P_{1B} & P_{1C} \\ P_{2A} & P_{2B} & P_{2C} \\ P_{3A} & P_{3B} & P_{3C} \\ P_{4A} & P_{4B} & P_{4C} \\ P_{5A} & P_{5B} & P_{5C} \end{bmatrix} \times \begin{Bmatrix} J_A \\ J_B \\ J_C \end{Bmatrix} \quad \Rightarrow \quad b = Ax$$

**A IS A NON SQUARED  
MATRIX AND NOT  
INVERTIBLE**

**We can solve to find the  
stiffnesses only if the  
matrix is square, i.e.,  
only if the number of  
unknown J's equals the  
number of  
measurements**



# Calculating Bridge Stiffness from deflection measurements

$$\begin{Bmatrix} \delta_1 \\ \delta_2 \\ \delta_3 \\ \delta_4 \\ \delta_5 \end{Bmatrix} = \begin{bmatrix} P_{1A} & P_{1B} & P_{1C} \\ P_{2A} & P_{2B} & P_{2C} \\ P_{3A} & P_{3B} & P_{3C} \\ P_{4A} & P_{4B} & P_{4C} \\ P_{5A} & P_{5B} & P_{5C} \end{bmatrix} \times \begin{Bmatrix} J_A \\ J_B \\ J_C \end{Bmatrix}$$

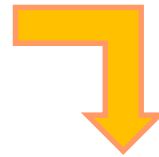
**The system of equations is also ill conditioned, i.e., even when the matrix is square, accuracy is very sensitive to noise in the measurement**



# Calculating Bridge Stiffness from deflection measurements

## Two problems:

- (i) Matrix not square,
- (ii) System is ill-conditioned



Moses algorithm  
+  
Penalty function



Moses algorithm minimises the differences between measured deflections and the theoretical response. It solves the problem of the non-square  $P$  matrix

Penalty function ensures that there is no sudden change of neighbouring stiffness values, avoiding, for example, negatives. It is based on a Blackman window. It solves the ill conditioning problem.



# Calculating Bridge Stiffness from deflection measurements

## Moses algorithm

$$E = \min[(\{\delta\} - [P]\{J\})^2]$$

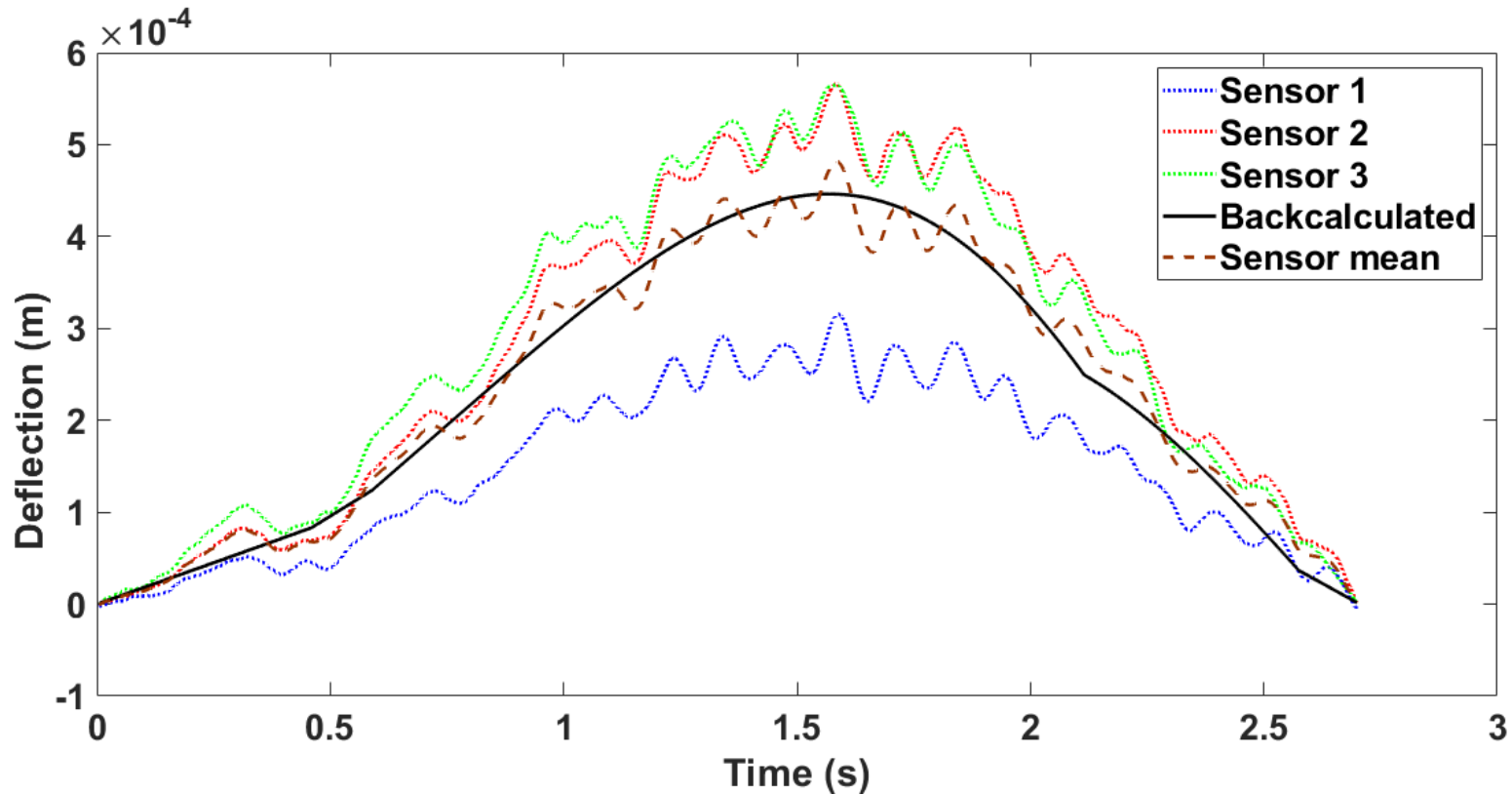
## Penalty Function

$$\sum_{i=1}^{n-1} k (-c_1 J_{i-b} - \dots - c_b J_{i-1} + J_i - c_{b+1} J_{i+1} - \dots - c_{2b} J_{i+b})^2$$

Where  $k$  is a set constant,  $b$  is the number of points used in the filter each side and the sum of constants  $c_1$  to  $c_{2b}$  equals 1



# Calculating Bridge Stiffness from deflection measurements





## Conclusions

- Deflection sensitivity to stiffness is greater at mid-span.
- Deflection data with loading conditions closer to mid-span should improve stiffness calculations.
- Moses and penalty function can potentially calculate stiffness decreasing the influence of noise.



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# Thanks for your attention

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